Preprint typeset in JINST style - HYPER VERSION

FERMILAB-PUB-15-104-ND

Design and operation of LongBo: a 2 m long drift liquid argon TPC

C. Bromberg[a], B. Carls[b], D. Edmunds[a], A. Hahn[b], W. Jaskierny[b], H. Jostlein[b], C. Kendziora[b], S. Lockwitz[b], B. Pahlka[b], S. Pordes[b], B. Rebel[b], D. Shooltz[a], M. Stancari[b], T. Tope[b] and T. Yang[b]

[a] *Michigan State University, East Lansing, Michigan 48824 USA*
[b] *Fermi National Accelerator Laboratory, Batavia, Illinois 60510, USA*

ABSTRACT: In this paper, we report on the design and operation of the LongBo time projection chamber in the Liquid Argon Purity Demonstrator cryostat. This chamber features a 2 m long drift distance. We measure the liquid argon purity using cosmic ray muons and the electron drift lifetime is at least 14 ms at 95% confidence level. LongBo uses cold electronics with discrete circuitry for the preamplifiers, and we measure a signal-to-noise (S/N) ratio of 30 at a drift field of 350 V/cm. An ASIC version of the cold preamplifiers was implemented on 16 readout channels, and we measure a S/N ratio 1.4 times larger for these channels.

KEYWORDS: LArTPC.

Contents

1. Introduction **1**

2. Construction of the LongBo TPC **2**

3. The High Voltage System **3**

4. Electronics **4**
4.1 Cold Electronics 4
4.2 Signal to Noise Ratio 5
4.3 Trigger 9

5. Operation **9**

6. Results **10**
6.1 Measurement of Electron Attenuation Using Cosmic Ray Muons 10
6.2 High Voltage Stability 16

7. Conclusions **16**

1. Introduction

Liquid argon time projection chambers (LArTPCs) provide excellent spatial and calorimetric resolutions for measuring the properties of neutrino interactions above a few MeV. Conventional liquid argon vessels, such as ICARUS [1], ArgoNeuT [2] and ARGONTUBE [3], *etc.*, are evacuated to remove water, oxygen and nitrogen contaminants present in the ambient air prior to filling with liquid argon. However, as physics requirements dictate larger cryogenic vessels to hold bigger detectors, the mechanical strength required to resist the external pressure of evacuation becomes prohibitively costly. The Liquid Argon Purity Demonstrator (LAPD) [4] was an R&D test stand at Fermilab designed to determine if electron drift lifetimes adequate for large neutrino detectors could be achieved without first evacuating the cryostat. The electron drift lifetime in this test measured with purity monitors was greater than 6 ms without initial evacuation of the cryostat; that lifetime exceeds the value of approximately 2 ms required for future large LArTPCs with drift distances on the scale of a few meters.

After achieving the required electron drift lifetimes, the LAPD cryostat was emptied and a TPC of 2 m drift distance, named LongBo, was installed in the central cryostat region. High liquid argon purity was achieved with the TPC in the cryostat. This paper summarizes the design and operation of the LongBo TPC.~~, which was the first TPC operated in the US to achieve a drift distance of 2 m.~~

2. Construction of the LongBo TPC

The LongBo TPC has a cylindrical sensitive volume with a 25 cm diameter and a 2 m length. LongBo extended the drift distance of the "Bo" TPC that was made a few years earlier with a 50 cm length [5]. LongBo has three sense wire planes, with wires oriented at 60 degrees from each other. There are 48 instrumented wires in each plane and the wires are 4.7 mm apart and made of 125 micron diameter beryllium copper. They were hand-soldered to a 3 mm thick copper-clad G10 board for each plane. The copper cladding was routed in a pad pattern on a Fermilab CNC router. A set of individual wires (shown with white insulation in figure 1) were soldered to the readout boards and terminated in a connector matched to a corresponding one on the preamplifier motherboards. The preamplifiers, often referred to as "cold preamplifiers" since they operated in the 87 K liquid argon, were placed around the TPC just outside the field cage. ~~; an arrangement dictated by the size of the cryostat flange on which the TPC was mounted. Olefin insulated flat cables took the signals from the motherboards to the signal feedthrough.~~ The wire planes were biased from external voltage sources via a feed through. The cathode was made from copper mesh, chosen to allow free argon flow along the TPC axis. The mesh was stretched inside a ring made of 19 mm diameter 3 mm thick stainless steel tube, which supports the TPC. A stainless steel tube elbow was welded to this ring and served to connect to the high voltage feed through, described in §3, via a cup and spring-finger connection.

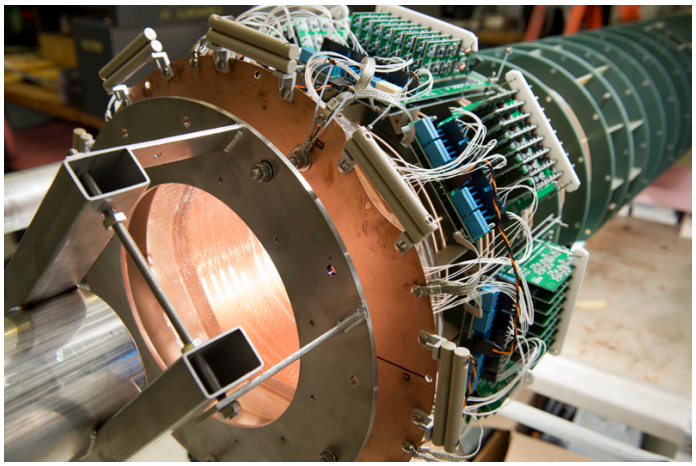


Figure 1: The wire planes and cold preamplifiers.

A uniform electric drift field was provided to the Bo TPC by a cylinder made of a copper-clad, 0.6 mm thick, G10 sheet, which is 50 cm long by 78 cm wide. The sheet was routed to create 18 mm wide copper strips, separated by 1.5 mm. The sheet was rolled into a 25 cm diameter tube which was inserted into a set of 7 rings routed from 4 mm thick G10. Two strings of 100 MOhm voltage divider resistors, Ohmite model 104, rated at 10 kV, 1 W, were soldered to the inner surface of the copper sheet. Only one string is necessary to create the electric field; the second is for redundancy. Figure 2 shows the resistors soldered to the inner surface of the copper sheet.

Bo was converted to LongBo by inserting three additional drift field sections, each 50 cm long, for a total drift length of 2 m. The drift field sections were connected together using threaded rod

Figure 2: The resistors soldered to the inner surface of the copper sheet.

to make the full 2 m drift cage. Beryllium copper spring stock were soldered to the ends of each cylinder to assure inter-connection at the joints. Figure 3 shows the assembled TPC with high voltage feedthrough and electronics.

3. The High Voltage System

To provide the electric field to drift the signal electrons, a high voltage was applied to the cathode mesh on the bottom of the TPC. The high voltage was generated outside of the cryostat by a Glassman LX150N12 power supply [6]. The supply was controlled remotely by a program and in normal operation, the current is much less than 1 mA. The supply was set to trip if more than 1.1 mA of current was drawn in order to protect the equipment and personnel who operate the system. Before entering the cryostat, the voltage was passed through a filter pot. This low-pass filter was a sealed aluminum vessel with cable receptacles that electrically connected to eight 10 MΩ resistors submerged in Diala oil. The capacitance for the filter was supplied by the cable to the feedthrough. The purpose of the pot was twofold: it reduced the high-frequency ripple from the power supply, and it limited the energy to the TPC in the case of a high voltage discharge.

A feedthrough transmits the high voltage into the cryostat and to the receptacle cup of the cathode plane. This feedthrough is shown in figure 4 and was modeled after the feedthrough used in the ICARUS experiment [1] with a stainless steel inner conductor insulated radially by ultra high molecular weight polyethylene (UHMW PE), and surrounded by a stainless steel ground tube. Grooves were added to the exposed UHMW PE to reduce surface currents. Initially, conducting shielding cups, shown in figure 4b, were installed to reduce the field along the feedthrough. Midway through running, the cups were removed to determine what effect they had on performance. No change was seen. To ensure good electrical contact, the feedthrough has a spring tip that is inserted into a receptacle cup attached to the cathode plane.

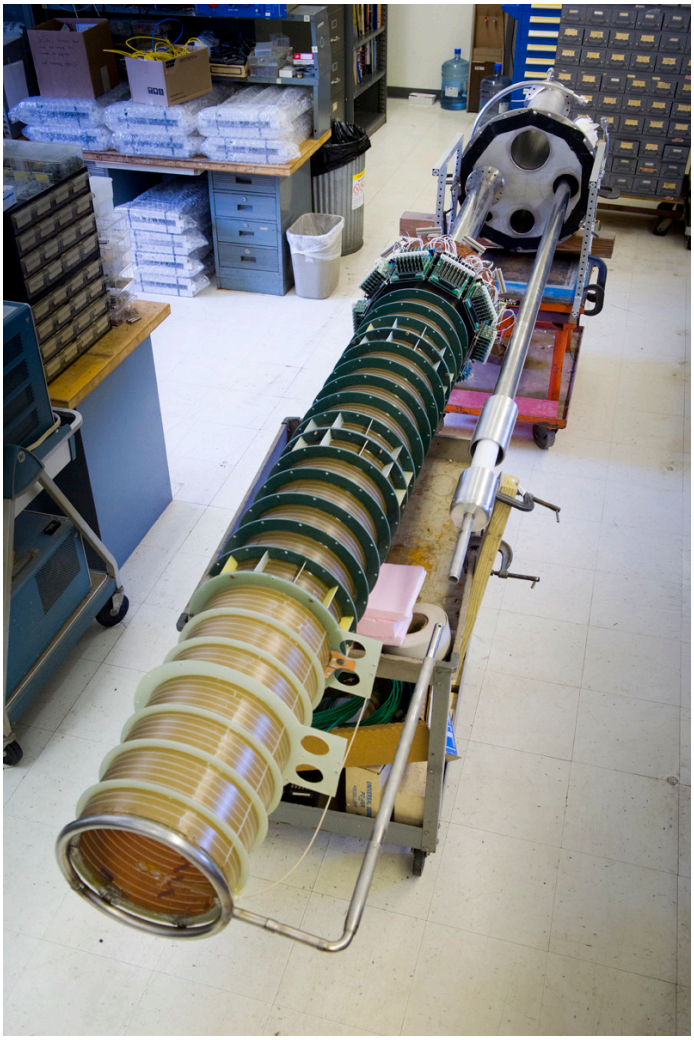


Figure 3: Assembled LongBo TPC.

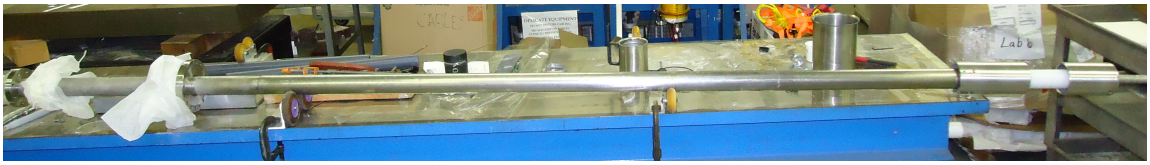
4. Electronics

4.1 Cold Electronics

The LArTPC technology was pioneered by the ICARUS collaboration using warm electronics with a dual-jFET charge integrating front-end preamp. For each wire of the ICARUS detector the feed-through passed DC bias-voltage into the cryostat and passed the TPC signals back to the electronics. Early development in the US used a similar warm preamplifier on a 3-plane LArTPC detector, Bo [5], built by Fermilab and used a 32-channel ADF2 digitizer built by MSU for the D0 experiment. At the same time the ArgoNeuT [2] LArTPC was built and used the same warm preamplifier design readout.

~~The readout electronics used in LongBo are the result of earlier development efforts by MSU for the Bo [5] and ArgoNeuT [2] TPCs. These systems employed preamplifiers positioned outside of the cryostat.~~ The development of cold electronics for a LArTPC was driven by fact that at the

(a)



(b)

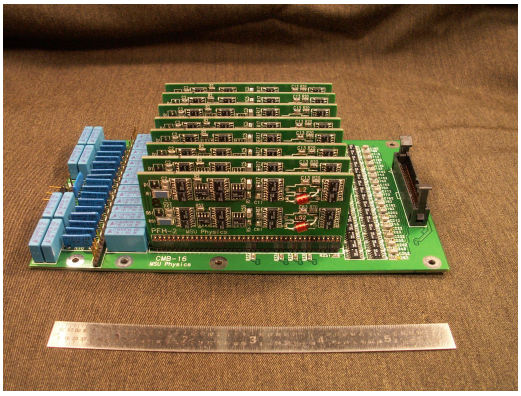
Figure 4: Photographs of the HV feedthrough without (a) and with (b) the electric field shielding cups.

87 K temperature of liquid argon there is less intrinsic noise in a MOSFET preamp than in the best warm preamp. Additionally, by mounting the preamp on the TPC the noise generated by a cable capacitance can be eliminated. Michigan State University (MSU) assembled 72 dual-channel hybrid preamplifiers designed for operation at 87 K, using a CMOS transistor chip front-end configured as a charge integrator, followed by a combination of high and low pass filters characterized by a step-function response with a 2.4 μs peaking time. The cold preamp-filter cards were first used by the Bo TPC to replace the original warm preamp-filters and then used by the LongBo TPC. Cold motherboards (CMB) each carrying 8 dual-channel hybrids, were mounted on brackets, as shown in figure 5, close to the wire planes. The 9 CMB boards read out 144 channels in total. Short insulated wires connected each CMB to a TPC wire plane. Flat Polyolefin cables carried the output of each CMB to a warm feedthrough. Cable drivers on the backside of the feedthrough drove signals to ADF2 digitizers sampling at 2 MHz.

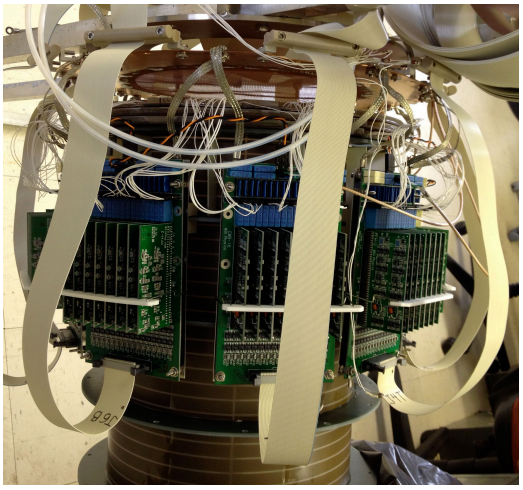
A MOSFET ASIC preamp-filter for use at cryogenic temperatures was designed by BNL [11] for DUNE [12]. It is also the readout of the TPC detector for the MicroBooNE experiment [13]. A version (V4) of this 16-channel ASIC became available in 2012 and was implemented for the LongBo TPC. One 16-channel preamp-filter card was modified to use a section of the MicroBooNE motherboard that serviced a single ASIC as a mezzanine board. The input/output connectors, bias-voltage distribution and decoupling capacitors of the card were retained. An ASIC control box was built which set the gain and peaking time parameters of the ASIC. The ASIC modified preamp-filter card was installed in place of one induction plane card with the signals processed by the same digitizing electronics.

4.2 Signal to Noise Ratio

The signal to noise ratio is an important metric of performance for a liquid argon detector. The absolute numerical value depends upon wire spacing, wire capacitance, readout electronics and drift field strength. Because 16 channels of the LongBo readout electronics were instrumented



(a) Cold motherboard.



(b) TPC with preamp-filters mounted.

Figure 5: Left: Cold motherboard with 8 preamp-filter cards. Right: TPC with preamp-filters mounted near the wire planes. The flat Polyolefin cables connect the output of the cold CMB cards to the cold side of the signal feedthrough card.

with the BNL ASIC preamplifier, a direct performance comparison can be made between the ASIC version of the preamplifier and the discrete CMOS version used for the remaining channels.

To measure the noise for each channel, a special run of 200 triggers was taken with a random trigger and no drift field. For each channel, the measured ADC counts for all 200 triggers were combined and the distribution fit to a Gaussian function. The width of the best fit Gaussian is reported as the noise in figure 6. The measured noise in Fig. 6 can also be determined from regular data runs with an external muon trigger and nominal drift field if signals from cosmic ray muons are removed from the acquired waveforms.

The signal strength was extracted from straight muon tracks acquired with the cosmic ray muon trigger, which is described in § 4.3. The signal to noise ratio of the discrete electronics chain was determined from signals on the collection plane wires. Clean tracks were selected from the first 200 triggers in each run considered using the event display. Only tracks whose projection onto the wire plane under study was nearly perpendicular to wire direction and centered on the wire plane were selected. The signal strength is recorded as the maximum ADC count in the waveform. The outermost two wires on either edge of the wire plane were excluded from the analysis as a fiducial volume cut intended to reject hits close to the field cage where the drift field may not be uniform and the pulse heights are noticeably reduced. In addition, wires exhibiting pulse heights greater than 1.5 times the average pulse height for the track were interpreted as delta rays and excluded. Finally, wires with more than one hit for a given trigger were excluded.

In the absence of diffusion, the length of the track segment that contributes to the signal on a particular collection plane wire is $\frac{\Delta w}{\sin(\theta)\cos(\phi)}$, where $\Delta w = 4.7$ mm is the wire spacing and θ and ϕ are the reconstructed track angles defined in § 6.1. The individual measured signal strengths were reduced by a factor of $\sin(\theta)\cos(\phi)$ before taking the average of all *good* collection wire values from the 10-12 event sample to obtain the value of the signal strength $S = 50.3$ ADC counts and a

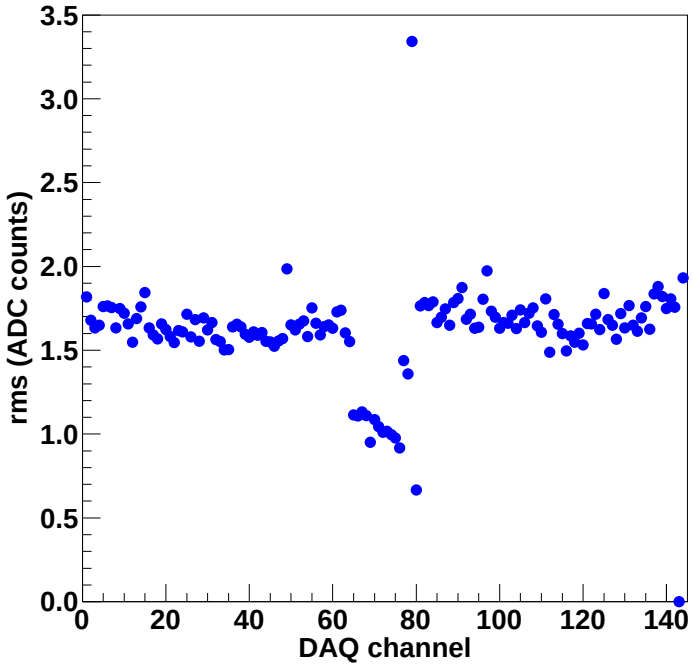


Figure 6: Measured noise as a function of DAQ channel number. Channels 1-48 are the first induction plane, channels 49-96 are the second induction plane and channels 97-144 are the collection plane. Channels 65-80 are instrumented with the BNL ASIC preamplifier, all other channels are instrumented with the MSU discrete CMOS preamplifier. After the first HV breakdown, four channels of the ASIC readout (channels 77-80) exhibited more noise than before and it was no longer possible to change their parameter settings. All of the MSU discrete CMOS channels survived the HV breakdowns.

signal to noise ratio of $50.3/1.69 \sim 30$ for the discrete CMOS electronics chain.

The signal to noise ratio provides a good comparison of the performance of the different amplifier flavors. The ASIC preamplifier is connected to the center 16 wires of the middle (induction) wire plane, so induction plane signals must be compared. For these bipolar signals, the signal strength used is the difference between the pedestal and the minimum ADC count of the waveform, or the depth of the dip in the bipolar signal shape. Tracks whose projection onto the middle wire plane is perpendicular to the wire direction were selected ($\phi \sim 60^\circ$) and the extracted sig-

nal strengths were normalized by the factor $\sin(\theta)\cos(\phi - 60^\circ)$. The ratio of the average signal strength for ASIC and discrete channels is reported in table 1 for different values of the shaping time constant. Both the measured noise and the signal to noise ratio increase with the shaping time constant.

Table 1: Comparison of signal and noise for discrete CMOS preamplifier and the ASIC preamplifier for different settings of the shaping time constant of the ASIC. The discrete CMOS preamplifiers have a fixed shaping time of 2 μs. The gain setting of the ASIC was 25 mV/fC for all measurements tabulated.

Shaping time (μs)	S	$S_{discrete}$	N	$N_{discrete}$	$(S/N)/(S/N)_{discrete}$
0.5	10.1	36.1	0.55	1.69	0.9
1.0	19.3	35.1	0.75	1.69	1.2
2.0	33.6	35.5	1.10	1.69	1.4
3.0	40.3	35.8	1.35	1.69	1.4

Figure 7 shows the shape of the amplified signal on a single wire for different shaping times, with the the signals scaled to have the same peak height to facilitate comparison. There is little if any difference in the pulse shapes - the shape is dominated by the width of the pulses before amplification. Changing the shaping time constant changes the overall gain of the amplifier.

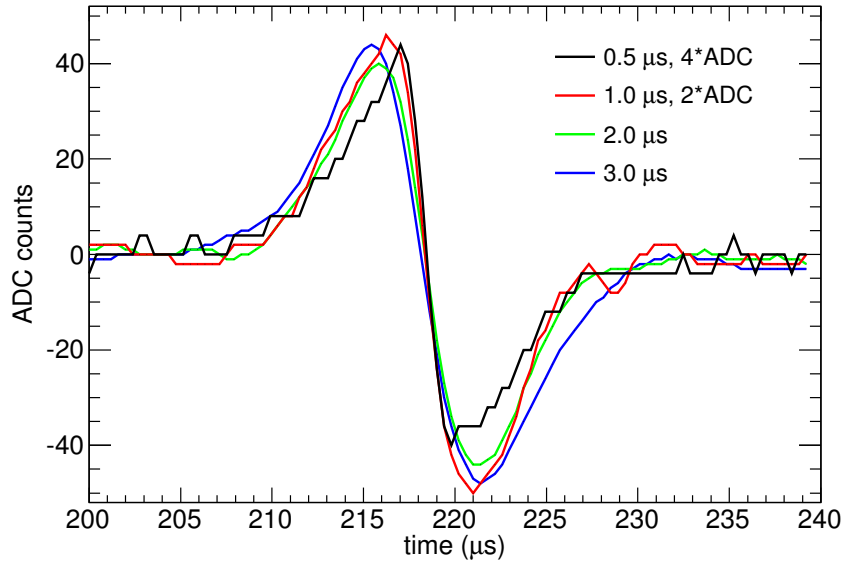


Figure 7: Raw signal shapes for induction plane signals with different settings of the ASIC shaping time constant are shown. The horizontal axis has an arbitrary zero so that the pulses are shown with the zero crossing point artifically aligned. The tracks from which these signals are taken form an angle of roughly 20 degrees with the plane of the wires, or $\theta \sim 70$. The angle between the projection of the track onto the wire plane and the wires themselves is ~ 80 degrees.

4.3 Trigger

The presence of through-going muons were detected by three sets of scintillation counters placed around the exterior of the LAPD cryostat as illustrated in figure 8. Each set consisted of two groups of counters placed on opposite sides of the cryostat, with the line intersecting the groups of counters passing roughly perpendicular to the wire direction for one wire plane. There were 8 counters (4 pairs) in each of the 6 groups, stacked in a column for an effective area of scintillator roughly 3 m by 0.4 m, for a total of 48 counters. One control and concentrator unit (CCU) controls 48 counters setting the gain of the photomultiplier tube (PMT) and a discriminator threshold [14]. A coincidence was required between counters on opposite side of the cryostat, and the track angle coverage is shown in § 6.1.

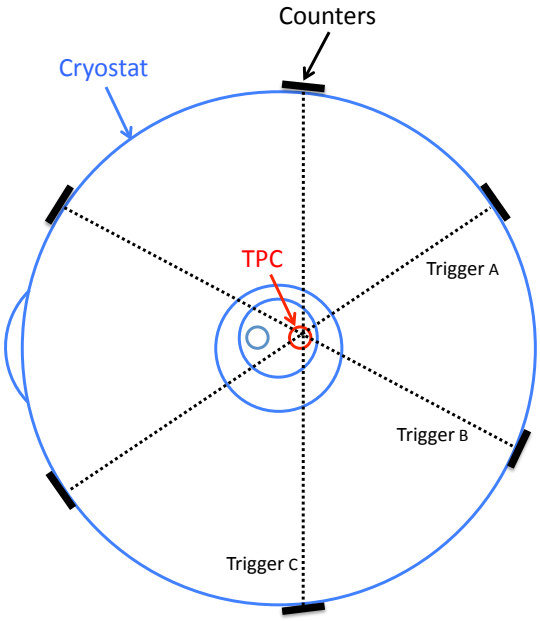


Figure 8: Location of the scintillation counters.

5. Operation

The LAPD cryostat is an industrial low pressure storage tank. The cryostat has a flat bottom, cylindrical sides, and a dished head. The cryostat diameter is 3.0 m and the cylindrical walls have a 3.0 m height. The LongBo TPC was inserted into the LAPD cryostat in October, 2012. Figure 9 shows the positions of the TPC and the high voltage feed through inside the LAPD cryostat. After purging the cryostat with argon gas and then filtering the argon gas for several days, as described in [4], the cryostat was filled with liquid argon. The high voltage was raised after the electron drift lifetime passed 0.3 ms. The TPC data taking lasted for 8 months.

An issue we encountered in the LongBo run was that the high voltage was unstable. The cause of the instability is unknown, but was present during the entire data-taking period. This

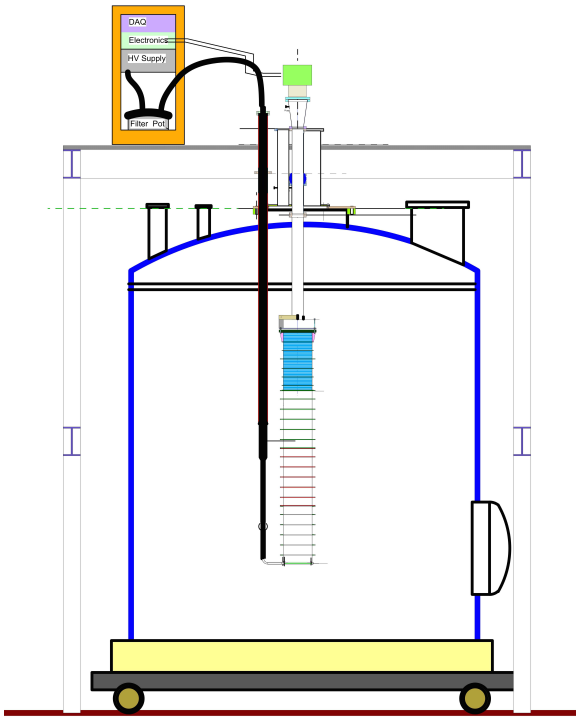


Figure 9: The TPC and high voltage feed through inside the LAPD cryostat.

instability forced the running of the TPC at a lower high voltage than desired, ultimately reaching a maximum -75 kV, with occasional trips, instead of the desired 100 kV for a 2 m drift TPC. Even with the lower-than-desired high voltage, several hundred thousand clear cosmic ray muon tracks were recorded. The data were used to study the electronics performance and liquid argon purity.

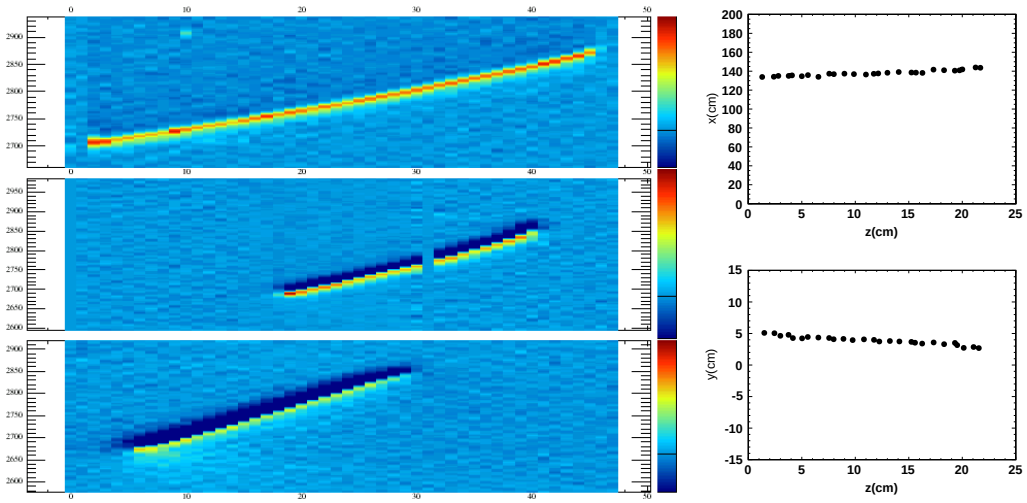
6. Results

6.1 Measurement of Electron Attenuation Using Cosmic Ray Muons

When cosmic ray muons pass through the liquid argon, they deposit energy through ionization and scintillation. The ionization electrons are drifted by the electric field and collected by the wire planes. The variation of the energy deposition along the muon track is small for the energetic muons. By examining the signal recorded by each wire as a function of electron drift time, one can measure the attenuation of ionization electrons along the drift distance and determine the electron drift lifetime. This method was used by ArgoNeuT to derive an electron drift lifetime [2].

We analyzed cosmic ray muon data taken during one full cycle of LAPD running, from when the liquid argon started recirculating through the filters to when it stopped. The high voltage we applied to the cathode was -70 kV during this period, which produced an electric field of 350 V/cm in the TPC volume. In this section, we present results on the measurements of electron attenuation using these data.

There are 491 966 triggered events during this run period. We use the LARSOFT software package [15] to reconstruct cosmic ray muon events. The automated reconstruction first converts the raw signal from each wire to unipolar pulse by removing electronics and electric field responses through deconvolution, and then finds hits by fitting a Gaussian to the resulting pulse. The hits from each plane of the TPC are grouped into clusters in drift time and wire number. Three dimensional tracks are constructed from pairs of line-like clusters in each plane. There are 274 491 events with at least one reconstructed track. Figure 10 shows one example event where a muon track is visible.



(a) Raw data (b) Reconstructed track

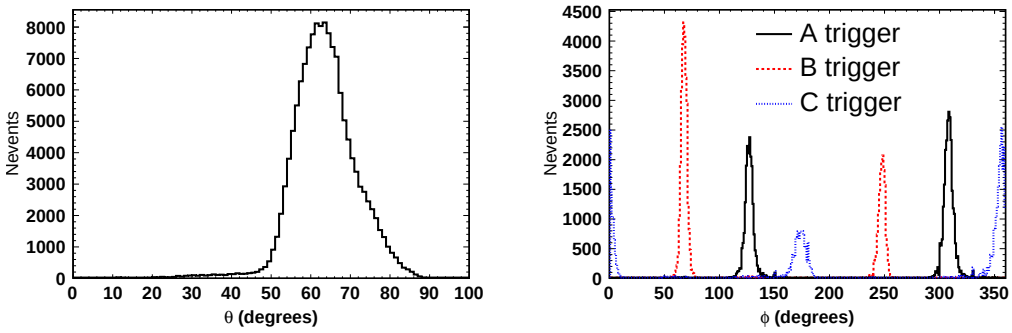
Figure 10: Run 293 Event 2225. (a) Drift time versus wire ID for raw wire signal from 3 wire planes. Red color represents large positive charge and blue color represents large negative charge. (b) Reconstructed track points in the x-z and y-z projections.

In this analysis we only consider the 223 194 events with exactly one reconstructed track that has at least 5 reconstructed 3-dimensional points along the track trajectory. We do not use events with multiple muon tracks because we cannot determine the track start time, t_0, for each track. Figure 11 shows the angular distributions of the reconstructed tracks. The track angle is determined by the reconstructed track start and end points, assuming the track is a straight line. The zenith angle θ is peaked around 60° and the azimuthal angle ϕ is determined by the trigger counter locations. Figure 12 shows the reconstructed track start point x, in the drift direction, versus the θ angle; $x = 0$ is near the wires. The muons normally enter the TPC in the middle, but they can be close to the wire planes and cathode.

The determination of the argon purity is performed using the collection plane hits on the track. We first select events with well reconstructed and clean tracks, where

1. the RMS distance of reconstructed 3D points with respect to a straight line determined by track start and end points should be less than 6.3 cm;

2. the number of hits that are not associated with the reconstructed track should be less than 11;



(a) Track θ (b) Track ϕ

Figure 11: Reconstructed track angles: (a) θ - with respect to the vertical direction, while $\theta = 0$ is at the zenith; (b) ϕ, events taken with different triggers have distinct ϕ distributions.

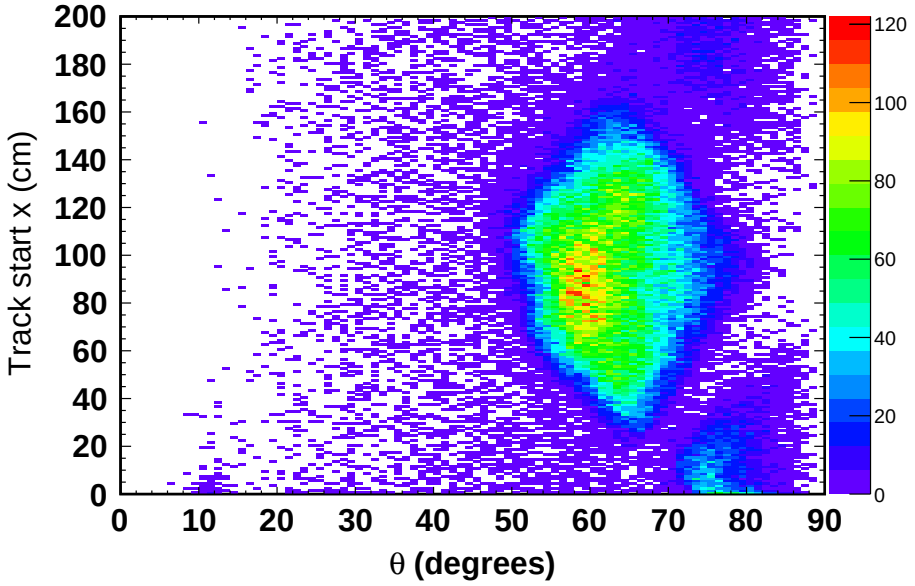


Figure 12: Reconstructed track start point in the drift direction (x) versus track angle (θ). The muons normally enter the TPC in the middle, but they can be close to the wire planes and cathode.

3. track length is required to be greater than 15 cm;

4. track length $\times \cos\phi$, the projection along the collection plane trigger direction, is required to be greater than 10 cm;

5. θ is required to between 50° and 70°.

The selection was chosen to maximize the good track fraction by scanning the distributions. We then select all hits on the collection plane associated with the tracks. We require only one hit on

each wire. If there is one hit on each of three contiguous wires that has $dQ/dx > 2000$ ADC/cm, we do not use those three hits. Both requirements are meant to remove delta rays.

For each selected hit, we look at raw wire signal for that hit in the region $[t-3\times\sigma, t+3\times\sigma]$, where t is the reconstructed hit time and σ is the reconstructed hit width. We first find the peak of the raw digits in ADC, we then sum all the digits above a threshold of 10% of the peak to get the charge of the hit. This threshold is chosen based on measured signal to noise ratio. By using raw wire signal we remove uncertainties introduced by signal shaping in the hit reconstruction. We then divide the hit charge by the track pitch, which is defined as the wire pitch over dot product of the track direction and the direction normal to the wire direction in the wire plane, to get dQ/dx for the hit.

Figure 13 shows the hit dQ/dx distributions when the electron drift lifetime was 0.4 ms (left) and 30 ms (right). The top plots show dQ/dx versus electron drift time distributions. The middle plots show the dQ/dx distributions for hits with drift time betwen 456 and 507 μs, indicated as gray bands in the top plots. We fit a Landau convoluted with Gaussian function to the dQ/dx distribution. The bottom plots show the most probable value (MPV) from the Landau fit as a function of drift time. The signal decreases as drift time increases as expected. We fit an exponential function to the data points:

$$dQ/dx = e^{-at_d+b}, \tag{6.1}$$

where t_d is the drift time and a is the attenuation constant. Figure 14 shows $dQ/dx_0 = dQ/dx(t = 0) = e^b$ as a function of time and the fluctuation is small.

Figure 15 shows the charge ratio

$$Q/Q_0 = e^{-\Delta t/\tau} = e^{-a\Delta t} \tag{6.2}$$

as a function of time. We use $\Delta t = 1$ ms, which is the typical time range in the TPC measurement. For comparison, we also convert the anode-to-cathode ratio (Q_A/Q_C) measurement by the purity monitor for a 0.31 ms drift time [4] to Q/Q_0 assuming a 1 ms drift time. The sources of systematic uncertainty on the purity monitor measurement are discussed in Ref. [4] and shown on the plot as a combined 15% absolute uncertainty on converted Q/Q_0.

In order to evaluate the systematic uncertainties on the purity measurement using TPC data, we test the same method using a sample of 100 000 simulated cosmic ray muon tracks in the LongBo TPC. The simulation was done with LARSOFT [15], and accounts for the energy and angular distribution of cosmic ray muons. The simulation includes the muon ionization and recombination effects, the free electron longitudinal and transverse diffusion, the signal attenuation due to the impurities in liquid argon and the electronic response. The method has been tested for electron lifetime in the 0.5 - 30 ms interval. The results show the measurement is reliable in a large range of liquid argon purity values and are used to correct the measured Q/Q_0 values to obtain the true Q/Q_0 values as shown in figure 15.

We consider two systematic effects in the purity measurement: field non-uniformity and system instability, which are described as follows.

It is possible that the electric field in the TPC is not completely uniform because of the possible broken resistors and the presence of the positive ions (space charge). However, we have evidence that the field uniformity is fairly well preserved:

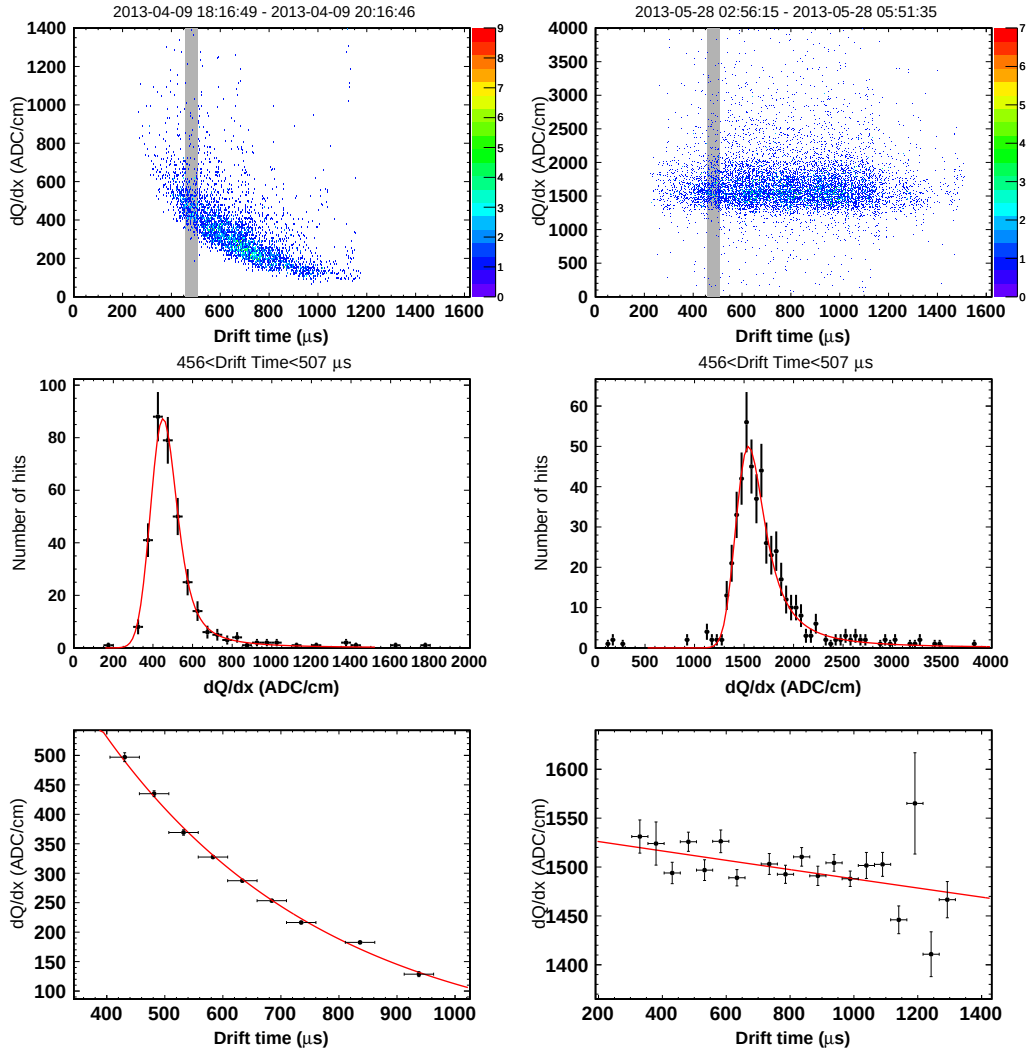


Figure 13: dQ/dx distributions of hits using data taken in two periods of time when the electron lifetime was 0.4 ms (left) and 30 ms (right), respectively. Top: Scatter plots of dQ/dx as a function of electron drift time; Middle: dQ/dx distributions for hits with drift time between 456 and 482 μs; Bottom: dQ/dx from Landau fit as a function of drift time.

- The maximum drift time we observe in the TPC data is consistent with the drift time for an electric field of 350 V/cm over 2 m.

- We do not observe large visible distortion of tracks.

The method we employ to measure the electron drift lifetime is largely insusceptible to random non-uniformity in the electric field. The measurement depends on the electron drift time, which is measured by the scintillation counter and the data acquisition system to a good precision (less than 1 μs) and is unaffected by the non-uniform electric field. We do not use signal recorded on the boundary wires to avoid edge effects near the field cage.

There is a 1% uncertainty in the high voltage applied to the cathode resulting from the power

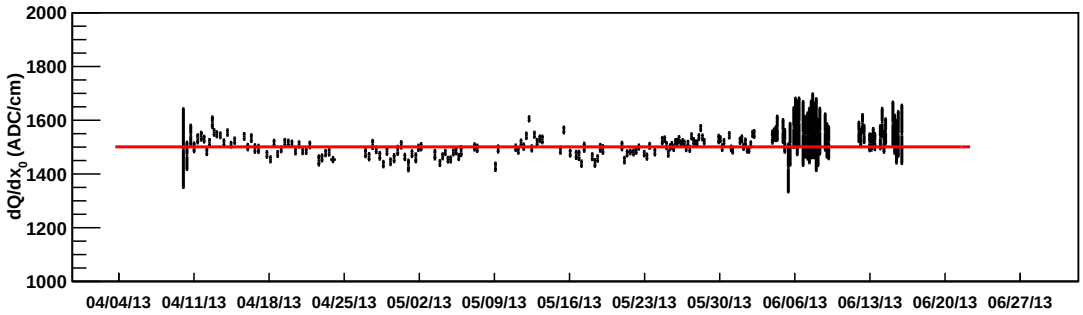


Figure 14: dQ/dx_0 as a function of time.

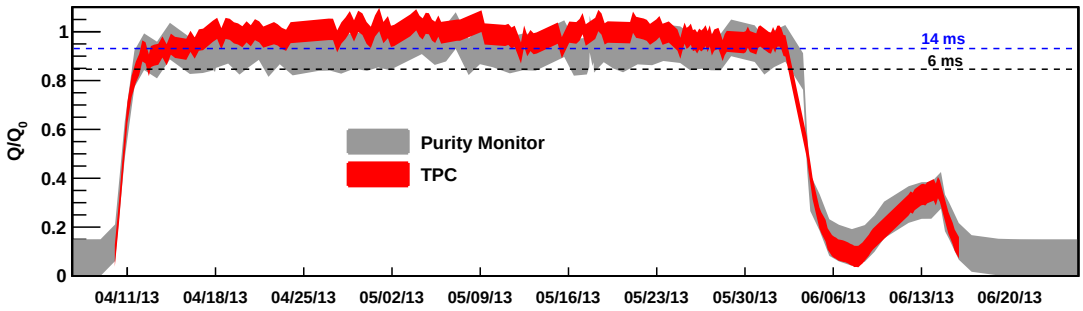


Figure 15: Comparison between Q/Q_0 measured by the TPC and the converted $Q_/Q_0$ using the purity monitor data. Q/Q_0 is a measure of the electron lifetime, and the values $\tau = 6$ ms and $\tau =$ 14 ms that correspond to Q/Q_0 = 0.85 and Q/Q_0 = 0.95, respectively, are indicated with dashed lines.

supply monitor and filter resistors. We vary the magnitude of the constant electric field by $\pm 5\%$ conservatively in the reconstruction code and the resulting difference in the Q/Q_0 is negligible.

The accumulation of space charge in the TPC can change the electric field in a way that affects the electron drift lifetime measurement directly. Ref. [7] predicts the electric field is increasing at longer drift distance as $\propto \sqrt{1+\beta x^2}$ where x is the drift distance with respect to the anode and β is a constant that depends on the chamber length, the applied high voltage and the cosmic ray rate. Because a larger electric field suppresses the electron-ion recombination, one expects more charge at longer drift distance, and the measured signal attenuation is smaller than the real attenuation in the presence of a space charge induced electric field distortion. We introduced a changing electric field in the simulation so the field at the cathode is 20% larger than the field at the anode. The resulting Q=Q0 is shifted by 0.03. Because we do not know what fraction of the argon ions were absorbed by the field cage before arriving at the cathode, take 0.03 as the systematic uncertainty from undetected non-uniformity in the drift field.

We also study the system instability by looking at the distribution of Q/Q_0 when the value is consistent with 1 (left of plot in figure 15). The distribution shows a mean value of 0.987 with a width of 0.03. We take 0.03 as systematic uncertainty from system instability. The total systematic

uncertainty is 0.04 and is shown in figure 15.

Following the Bayesian approach we set a lower limit on Q/Q_0 to be 0.932 at 95% confidence level, which corresponds to a lifetime of 14 ms.

6.2 High Voltage Stability

The power supply was set to turn off if it drew an over-current much greater than the operating current of the TPC. During data taking, the cathode high voltage never sustained greater than 80 kV for a significant period with most data being collected with 60 or 70 kV on the cathode. A correlation was noted between greater high voltage stability and greater electronegative contamination in the argon. This trend can be seen in figure 16 where the number of high voltage trips is displayed along with a purity monitor reading as a function of time. While a precise characterization of the dependence is beyond the scope of this paper, the behavior agrees with other studies in the literature that have shown a trend between an increase in electronegative contamination and an increase in liquid argon's dielectric strength [8, 9, 10].

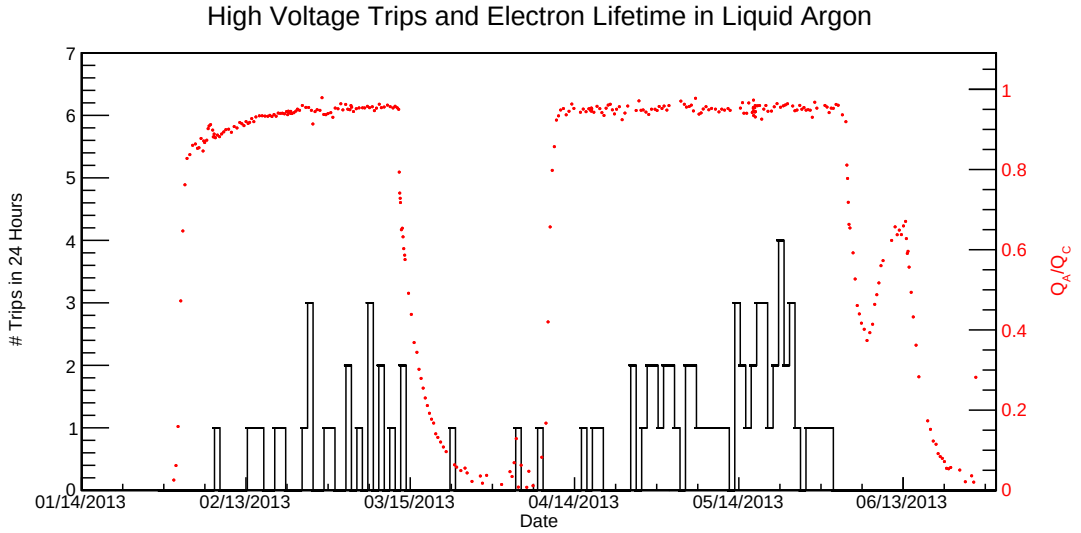


Figure 16: The number of cathode high voltage trips in a 24 hour period and purity monitor values during data taking. The trip counts are given by the black solid line and scale on the left. Trips related to testing the high voltage system were not included in the trip count. A quantification of the argon purity is given by the red dots and the scale on the right, which is the ratio of the anode signal to the cathode signal measured by the purity monitor.

7. Conclusions

In this paper we have discussed the design and operation of the LongBo TPC in the LAPD cryostat. A ratio $S/N = 50.5/1.69 \sim 30$ was measured for the wires in the collection plane with discrete CMOS electronics. For these data the TPC was operated with a drift field of 350 V/cm. The measured S/N ratio for the ASIC channels was 1.44 times larger than that measured for the discrete channels for the ASIC shaping time of 2.0 μs and a gain setting of 25 mV/fC. The liquid argon

purity measurement using cosmic ray muons in the TPC shows the electron drift lifetime is at least 14 ms at 95% confidence level for a long period of time. We also observe a correlation between the voltage stability and the liquid argon purity.

Acknowledgments

We would like to thank Tom Junk for the useful discussions on statistical analysis. This work was supported by the US DOE, and by the NSF through Grants 1068318 and 1410972, to Michigan State University. We thank the staff at Fermilab for their technical assistance in running the LAPD experiment. Fermilab is operated by Fermi Research Alliance, LLC under Contract No. De-AC02-07CH11359 with the United States Department of Energy.

References

[1] S. Amerio et al. (ICARUS Collaboration), *Design, construction and tests of the ICARUS T600 detector*, *Nucl. Instrum. Meth. A* **527**, (2004) 329.

[2] C. Anderson et al. (ArgoNeuT Collaboration), *The ArgoNeuT detector in the NuMI low-energy beam line at Fermilab*, 2012 *JINST* **7** P10019.

[3] A. Ereditato, *et al.*, *Design and operation of ARGONTUBE: a 5 m long drift liquid argon TPC*, 2013 *JINST* **8** P07002.

[4] M. Adamowski et al., *The Liquid Argon Purity Demonstrator*, 2014 *JINST* **9** P07005.

[5] C. Bromberg, *First neutrino physics results of the ArgoNeuT experiment, and first tracks with CMOS preamplifiers operating at 87 K*, in Proceedings of the 2nd International Workshop towards the Giant Liquid Argon Charge Imaging Experiment (GLA2011), 5-10 Jun 2011, Jyväskylä, Finland, lartpc-docdb.fnal.gov/0008/000819/001/CBromberg_GLA2011_Proc.pdf, to be published.

[6] Glassman High Voltage Inc., PO Box 317, 124 West Main Street, High Bridge, NJ 08829-0317, U.S.A. www.glassmanhv.com.

[7] S. Palestini et al., *Space charge in ionization detectors and the NA48 electromagnetic calorimeter*, *Nucl. Instrum. Meth. A* **421** 1999 75.

[8] D. Swan and T. Lewis, *Influence of electrode surface conditions on the electrical strength of liquified gases*, *J. Electrochem. Soc.* **107** (1960) 180.

[9] A. Blatter et al., *Experimental study of electric breakdowns in liquid argon at centimeter scale*, 2014 *JINST* **9** P04006.

[10] R. Acciarri et al., *Liquid argon dielectric breakdown studies with the MicroBooNE purification system*, 2014 *JINST* **9** P11001.

[11] C. Thorn et al., *Cold Electronics development for the LBNE LAr TPC*, *Phys. Procedia* **37** (2012) 1295.

[12] C. Adams et al. (LBNE Collaboration), *The Long-Baseline Neutrino Experiment: exploring fundamental symmetries of the universe*, `hep-ex/1307.7335`.

[13] http://www-microboone.fnal.gov/publications/TDRCD3.pdf.

[14] C. Bromberg, *Gain and threshold control of scintillation counters in the CDF muon upgrade for Run II*, *Int. J. Mod. Phys. A* **16S1C** (2001) 1143.

[15] https://cdcvs.fnal.gov/redmine/projects/larsoft. We use version v02_00_01 of this software package.

[16] K.A. Olive et al. (Particle Data Group), *Chin. Phys. C* **38** (2014) 090001.